PDE Backstepping Control of Congested Traffic

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Oil Drilling



Highway (single-lane) for gas, water, oil, mud, rock cuttings

Choke valve = ramp metering



Control of Flow Dynamics in CONGESTED Traffic

Suppressing STOP-AND-GO oscillations

(coupled PDEs)

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Keeping SHOCKS from drifting upstream (ODE with delays)

Control of Flow Dynamics in CONGESTED Traffic

Suppressing STOP-AND-GO oscillations (coupled PDEs)

Keeping SHOCKS from drifting upstream (ODE with delays)

Maximizing flow through BOTTLENECK (extremum seeking)



Ramp metering, flow rate actuated





Ramp metering, flow rate actuated Varying speed limit, velocity actuated

PDE Backstepping Control of Stop-and-Go Traffic

Aw-Rascle-Zhang model

 $\rho(x,t) = \text{traffic density}, v(x,t) = \text{traffic speed}$

LWR model
$$\partial_t \rho + \partial_x (\rho v) = 0$$

$$\partial_t (v + p(\rho)) + v \partial_x (v + p(\rho)) = \frac{V(\rho) - v}{\tau}$$

second-order, macroscopic, nonlinear hyperbolic PDEs

Freeway traffic open-loop simulation

$$\rho^{\star} = 120 \text{ vehicles/km}, \quad v^{\star} = \frac{22 \text{ mph}}{L} = 500 \text{ m}, \quad \tau = 60 \text{ s}$$



eigenvalues in RHP

Control objective

$$\rho(x,t), v(x,t)$$

$$\rho^{\star}, v^{\star}$$



Linearized ARZ model

 $\tilde{\rho}(x,t) = \text{density disturbance}, \tilde{v}(x,t) = \text{speed disturbance}$

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Linearized ARZ model

 $\tilde{\rho}(x,t) = \text{density disturbance}, \tilde{v}(x,t) = \text{speed disturbance}$

$$\tilde{\rho}_t + v^* \tilde{\rho}_x = -\rho^* \tilde{v}_x$$

$$\tilde{v}_t - (\gamma p^* - v^*) \tilde{v}_x = -\frac{\tilde{v} + \tilde{p}}{\tau}$$
• density disturbance $\tilde{\rho}$ "propagates" at traffic speed setpoint v^*
• speed disturbance \tilde{v} "counter-propagates" at $\gamma p^* - v^*$

Coupled 2×2 hyperbolic PDE model



Positive feedback throughout the domain

green/red light
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at downstream ramp

Theorem. Full-state feedback control law

$$U_{\text{out}}(t) = -r_0 \rho^* (v(L,t) - v^*) + r_0 \rho^* \int_0^L \left[M(L-\xi) - r_0 K(L,\xi) \exp\left(\frac{\xi}{\tau v^*}\right) \right] (v(\xi,t) - v^*) d\xi + k_0 \int_0^L K(L,\xi) \exp\left(\frac{\xi}{\tau v^*}\right) (\rho(\xi,t)v(\xi,t) - \rho^* v^*) d\xi,$$

makes equilibrium $\overline{w} \equiv \overline{v} \equiv 0$ exponentially stable in L_2 and equilibrium reached in finite time $t = t_f$.

Kernel equations

$$(\gamma p^{\star} - v^{\star})K_x - v^{\star}K_{\xi} = c(\xi)K(x - \xi, 0)$$
$$K(x, x) = -\frac{c(x)}{\gamma p^{\star}}$$

where $\{0 \le \xi \le x \le L\}$

$$M(x) = -K(x,0)$$

Full-state feedback simulation



Boundary observer for traffic estimation

Boundary measurement (of velocity and flow):

 $Y(t) = \bar{w}(\boldsymbol{L}, t)$

Observer

$$\hat{w}_t = -v^* \hat{w}_x + r(x)(Y(t) - \hat{w}(L, t))$$
$$\hat{v}_t = (\gamma p^* - v^*) \hat{v}_x + c(x) \hat{w} + s(x)(Y(t) - \hat{w}(L, t))$$
$$\hat{w}(0, t) = -r_0 \hat{v}(0, t)$$
$$\hat{v}(L, t) = r_1 Y(t) + U(t)$$

Density and velocity estimates



Data validation of boundary observer

Next Generation Simulation (NGSIM) traffic data I-80 in California



Traffic density and velocity for 5:15 pm - 5:30 pm



Estimation errors of boundary observer



Two-lane and Two-class traffic congestion control

Two-lane and Two-class traffic congestion control



Lane changing segregates drivers into the more "risk-tolerant" ones in the fast lane and more "risk-averse" ones in the slow lane.

Two-lane and Two-class traffic congestion control



Lane changing segregates drivers into the more "risk-tolerant" ones in the fast lane and more "risk-averse" ones in the slow lane. Mixed vehicle types induce creeping effect where the slow and bulky vehicles block the traffic and small and fast vehicles getting through.

Two-laneARZ modelIane changes ~ heat exchanger

Coupled 4×4 **nonlinear first-order hyperbolic PDEs**

$$\partial_t \rho_f + \partial_x (\rho_f v_f) = \frac{1}{T_s} \rho_s - \frac{1}{T_f} \rho_f$$
$$\partial_t (\rho_f v_f) + \partial_x (\rho_f v_f^2) - (\rho_f \gamma p_f) \partial_x v_f = \frac{1}{T_s} \rho_s v_s - \frac{1}{T_f} \rho_f v_f + \frac{\rho_f (V(\rho_f) - v_f)}{T_f^e}$$
$$\partial_t \rho_s + \partial_x (\rho_s v_s) = \frac{1}{T_f} \rho_f - \frac{1}{T_s} \rho_s$$
$$\partial_t (\rho_s v_s) + \partial_x (\rho_s v_s^2) - (\rho_s \gamma p_s) \partial_x v_s = \frac{1}{T_f} \rho_f v_f - \frac{1}{T_s} \rho_s v_s + \frac{\rho_s (V(\rho_s) - v_s)}{T_s^e}$$

Two-class ARZ model

Coupled 4×4 nonlinear first-order hyperbolic PDEs

$$\partial_{t}\rho_{1} + \partial_{x}(\rho_{1}v_{1}) = 0$$

$$\partial_{t}(v_{1} + p_{1}(AO)) + v_{1}\partial_{x}(v_{1} + p_{1}(AO)) = \frac{V_{e,1}(AO) - v_{1}}{\tau_{1}}$$

$$\partial_{t}\rho_{2} + \partial_{x}(\rho_{2}v_{2}) \neq 0$$

$$\partial_{t}(v_{2} + p_{2}(AO)) + v_{2}\partial_{x}(v_{2} + p_{2}(AO)) = \frac{V_{e,2}(AO) - v_{2}}{\tau_{2}}$$
"Area Occupancy" $AO(\rho_{1}, \rho_{2}) = \frac{a_{1}\rho_{1}(x,t) + a_{2}\rho_{2}(x,t)}{W}$

Coupled 4×4 nonlinear first-order hyperbolic PDEs



2+2 coupled PDE system

3 + 1 coupled PDE system

Two-lane traffic full-state feedback simulation



Two-class traffic full-state feedback simulation



 $Class1 \ small \ and \ fast$

Bilateral Boundary Control of Moving Shockfront



LWR traffic model

$$\frac{\partial}{\partial t}\rho_{\rm f} = -v_m \frac{\partial}{\partial x} \left(\rho_{\rm f} - \frac{\rho_{\rm f}^2}{\rho_m}\right)$$

density of "FREE traffic" (upstream of shock)

LWR traffic model

$$\frac{\partial}{\partial t}\rho_{\rm f} = -v_m \frac{\partial}{\partial x} \left(\rho_{\rm f} - \frac{\rho_{\rm f}^2}{\rho_m}\right)$$
$$\frac{\partial}{\partial t}\rho_{\rm C} = -v_m \frac{\partial}{\partial x} \left(\rho_{\rm C} - \frac{\rho_{\rm C}^2}{\rho_m}\right)$$

density of "CONGESTED traffic" (downstream of shock)

LWR traffic model

y of "FREE traffic" pstream of shock)

nock front location

(Rankine-Hugoniot jump condition)

Bilateral predictor-based control

$$U_{\text{in}}(t) = K_{\text{f}} \left[X(t) - \frac{b}{u} \left(\int_{0}^{l(t)} \tilde{\rho}_{\text{f}}(\xi, t) d\xi + \int_{l(t)}^{\min\{L, 2l(t)\}} \tilde{\rho}_{\text{c}}(\xi, t) d\xi \right) \right]$$
$$U_{\text{out}}(t) = K_{\text{c}} \left[X(t) - \frac{b}{u} \left(\int_{l(t)}^{L} \tilde{\rho}_{\text{c}}(\xi, t) d\xi + \int_{\max\{0, 2l(t) - L\}}^{l(t)} \tilde{\rho}_{\text{f}}(\xi, t) d\xi \right) \right]$$
PREDICTION of shock position over the CONGESTED/downstream segment

Microscopic simulation experiment in AIMSUN



uncontrolled

Open-loop becomes fully congested after 25 minutes

Microscopic simulation experiment in AIMSUN



shockwave of

closed-loop stopped at 1600 m, leaving upstream traffic in free regime.

Extremum Seeking Control of Downstream Traffic Bottleneck

Downstream traffic bottleneck



Downstream traffic bottleneck



Upstream traffic dynamics with $q_{in}(t) = Q(\rho(0, t))$

$$\partial_t \rho + \partial_x(Q(\rho)) = 0$$

Unknown quadratic map of bottleneck area

$$q_{\text{out}}(t) = Q_B(\rho(L, t)) = q^{\star} + \frac{H}{2}(\rho(L, t) - \rho^{\star})^2$$

Extremum Seeking Control with delay







Thanks for your attention!

